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Optimal Intertwine Transformer-based CLLC Resonant Circuit for Electric Vehicles On-Board Charging Applications

Vipul Gupta^{1*}, Dr. Bhoopendra Singh² and Dr. Sachin Tiwari³

¹Research Scholar, Department of Electrical and Electronics Engineering University Institute of Technology RGPV, Bhopal, Madhya Pradesh 462033, India. ²Associate Professor, Department of Electrical and Electronics Engineering University Institute of Technology RGPV, Bhopal, Madhya Pradesh 462033, India. ³Professor, Department of Electrical and Electronics Engineering

Lakshmi Narain College of Technology Excellence (LNCTE), Bhopal, Madhya Pradesh 462021, India. *Corresponding Author Email: vipulguptaap@gmail.com

Abstract

The proposed approach integrates an optimized transformer in an LLC resonant circuit for onboard charging in electric or hybrid electric vehicles (EVs or HEVs). The transformer is designed using an advanced optimization method, Horse Herd Optimization Algorithm (HOA), to minimize core loss, winding loss, and overall cost. A 3D model of the transformer is created and its performance is validated using MATLAB and ANSYS software. The proposed model achieves high power temperature, quality, low and low manufacturing cost. It outperforms other existing algorithms in terms of core loss and cost. The proposed model is well-suited for onboard charging applications in EVs or HEVs.

Keywords: Onboard charger; CLLC resonant circuit; integrated transformer; core loss; horse herd optimization.

1. INTRODUCTION

Electric vehicles (EVs) are gaining popularity due to rising oil prices and concerns about oil supplies. Onboard chargers are being explored as a way to enhance EV acceptance, especially for lightweight urban EVs. Phase-Shifted Full-Bridge (PSFB) and LLC resonant converters are commonly used in onboard charging systems. While PSFB converters offer wide voltage adjustment, LLC resonant converters have advantages in achieving higher performance. However, there are challenges and drawbacks associated with both types. The manuscript is organized into sections discussing related work, the proposed transformer modeling, results and comparison, and overall conclusions.

2. RELATED WORK

The literature review highlights various approaches aimed at improving power quality and enhancing the on-board charging capabilities of electric vehicles (EVs). Jothimani et al. [11] proposed a power factor correction modifier based on Interleaved Negative the Output Elementary Luo converter to ensure stable operation under load power variations. Taghizadeh et al. [12] presented an integrated control system for a multipurpose EV charger, addressing challenges such as charging/discharging, voltage regulation, and harmonic reduction. Zou et al. [13] developed a single-phase onboard charger that recycles traction inverter and motor, enabling increased voltage charging. Dao et al. [14] proposed a hybrid LLC resonator converter with three

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working modes to enhance performance under different load conditions. To address these drawbacks, a novel on-board charging method for EV applications will be introduced in the subsequent section.

2.1. Proposed model for improving PQ in EV's on-board charging application

The integrated dual-output DC/DC converter is commonly used for onboard charging in electric vehicles. To improve power quality and overcome drawbacks like high peak current, the proposed model introduces an integrated transformer topology that intertwines the LLC resonant converter.



Fig.1 Schematic diagram of the proposed model

2.2. Vehicle to grid operation

Figure 2 depicts the circuit topology of a CLLC resonant converter during the charging period.



Fig. 2 During G2V charging, the circuit architecture of a half-bridge CLLLC resonant converter

During this time, synchronous rectification upon that tertiary side is unplugged, and switches (S_9 and S_{10}) on the LV side are switched off. The power transmission occurs from the input voltage (V_{in}) to the primary side of the transformer via switches S_1 and S_2 .

2.2.1. G2V operation

For V2G operation, the full-bridge rectifier upon that tertiary side is still shut by switching off S_9 and S_{10} . The half-bridge CLLLC resonant converter, as seen in Fig. 3, which works in the opposite direction.



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Fig. 3 The half-bridge CLLLC resonant converter's circuit architecture for V2G operation



Fig.4 Flow chart of the proposed method for parameter selection

3. RESULT AND DISCUSSION

Table 1 summarizes the optimal ranges of transformer modelling variables.

Variables	Proposed HOA	MA	ALO	
Window	10.04 mm	17.29	20.09	
Area	10.04 11111	mm	mm	
No. of	700	820	780	
strands				
Diameter				
of a	79.5 mm	50.75mm	50.75mm	
conductor				
Volume of	75.09 cm^3	60.4 cm^3	58.5 cm3	
core	75.07 CIII	00. 4 CIII		

		~		c		
Table	1.	Com	parison	of (optimal	value

The parameter ranges of the proposed model are outlined in Table 2, and Figure 5 illustrates the convergence curve.

Table 2 provides a comparative analysis of fitness functions.



Fig. 5 Comparative analysis of fitness function

Table 2. Comparison of fitness function

Techniques	No. of	Fitness
НОА	95	850
МА	100	875
ALO	81	890

i) Finite element analysis of the proposed model



Fig.6 Core loss

The observed core loss is illustrated in figure 1. The peak value of the core loss is considered as 110 kW that is reached at 21st ms. After that, the loss is gradually decreased to reach 2 W at the 83rd ms. The proposed model provides a good power quality due to low core loss.

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(b)

Fig.7 Current and voltage flows of winding 1 and 2

In Figure 7, the proposed model illustrates the current and voltage waveforms of winding 1 and 2 for the transformer. The proposed model provides a stable current and voltages with low temperatures.



Fig.8 Flux linkages of winding 1 and 2





Figure 9 demonstrates the induced voltage waveforms of winding 1 and 2, it shows winding 1 induced voltage is higher than the winding 2 induced voltage.



Fig.10 Analysis of excess loss of proposed model

Then the proposed optimal core based transformer model's excess losses are analysed which is sketched in figure 10.



Fig.11 Analysis of stranded loss

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The stranded loss of the proposed optimal transformer was shown in figure 11.



Fig.12 Inductance leakage analysis of the proposed HOA model

At last the total winding resistance of the proposed HOA transformer is observed and plotted in figure 12.The analysis values show at the variation of frequency cause an improvement in winding resistance capacity. That is the proposed transformer provides 0.0161 Ω at the 10⁵ Hz frequency.





2.3. Comparative analysis

GA based optimal designing of the transformer provide high core losses, it contains 13.2 W. Similarly, HTS winding

model have 64.52 W core loss. Another method of two electrical steels combined model have4.15 kW core loss, M5-type silicon steel core model provides 401 W core loss at power transferring period, Harmonic field model of transformer provides 12.41 kW core loss. But in the proposed approach, the core loss contains 2 W which is demonstrated in table 3.

Table 3. Comparison of core loss

Techniques	Core loss	
HTS winding [22]	64.52 W	
GA based transformer [13]	13.2 W	
Two electrical steels [23]	4.15 kW	
M5-type silicon steel core [24]	401 W	
Harmonic field model [25]	12.41 kW	
Proposed optimal transformer	2 W	

3. CONCLUSION

The proposed approach integrates an optimal transformer using the Horse Herd Optimization Algorithm (HOA) into a CLLC resonant circuit for on-board charging applications. The transformer design is crucial for reducing costs and losses. The proposed model exhibits fast convergence and improved power quality with low cost and loss. MATLAB and ANSYS software are utilized to develop and validate the performance of the transformer. The 3D model of the transformer is created using ANSYS, and its mesh and temperature contour are validated. The performance is compared to other existing methods, and the proposed

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optimal transformer demonstrates superior results, such as a low core loss of 2W.

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