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GRID-CONNECTED CONVERSION OPTIMIZATION FOR DISTRIBUTED GENERATION IN UNBALANCED SYSTEMS DURING DISRUPTIONS

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ABSTRACT: Utilizing grid-connected conversions (GCCs) to maintain voltage level while riding over network disturbances has recently become one of the main needs reflected in grid rules. This study presents a novel method for injecting an appropriate set of +ve/-ve watt/wattles currents through four regulating variables to provide a reference signal that can sustain voltage levels. In order to determine the best configurations for all mesh voltage conditions, empirical formulas are offered. In order to achieve optimal performance, the following goals can be fulfilled: The phase voltage limitations were satisfied first, followed by an optimization of the flow of real and reactive power, a restriction of fault currents, and a reduction in real and reactive power oscillations. The development of GCCs can profit greatly from these ideal behaviors, which include increased efficiency, less dc-link disturbances, improved ac network stability, and a decrease in device failure. The suggested phrases and analytical results are validated by empirical studies and simulation.

Key words: generators of reference current, LVRT, converters, and grid failures.

1. Introduction

The growing integration of non conventional sources of energy and distributed energy (DG) equipment into power system networks has created serious stability concerns. As a result, undertake to ensure have developed strict criteria enabling GCCs to function under abnormal grid conditions [1–3]. As a result, GCCs must also withstand such disturbances and maintain grid supply, as well as provide v/f support. The compatibility of the grid-connected converters with these new criteria has just been extensively researched in the research. The study utilises, but modifies, one of most sophisticated RCG (reference current generator) method (described in [4]), which may include positive/negative and watt/wattles current flow with varying degrees of flexibility.

This RCG provides significant voltage support services by balancing the +ve and -ve sequences of the respective watt and wattles currents via two regulating parameters, kp and kq. Additionally, the real and reactive power control parameters could be regarded as the other two standard values.

The first section of this study provides extensive mathematical model to evaluate the effectiveness of the RCG used. Following phrases can assist engineers in properly designing a GCC's control systems. Optimum cycles on sudden real/reactive energies (pmax&qmax) and peak step currents are the three most important features of RCG techniques (Imax). The equations of pmax, qmax, and Imax for the applied RCG are developed in this article. This work's analytical analyses and principles may be used to a variety of approaches.

The main contribution of this work is a novel control system based on mathematical formulations that can determine the optimal ranges for the controlling (kp, kq, P, and Q) standard parameters in any fault condition state in order to achieve the desired goals:

1) decreased real and reactive power fluctuations; 2) increased and semi-balanced voltage levels at the PCC ; and 3) reduced leakage currents of the inverter.

For entirely realise such purposes, the formulas for enhanced grid voltage, optimum fluctuations on simultaneous real/reactive values, and highest



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component currents under imbalance conditions must be determined.

The maximum possible support is suggested as a the second commitment to acquire the most possible watt and wattles power that the device can give to the power system beneath irregular system disturbances without reaching the maximum possible instantaneous phase current restriction. The MAS monitoring system strives to provide optimal grid voltage or/and frequency assistance while also adhering to the upper allowed of phase currents defined by the GCC grading.

Section III further derives and provides the theoretical formulations of the MAS regulate techniques for the diverse situations, such as diverse abnormal types, voltage drop peculiarities, many network constraints, node mobility, and so on. The proposed statements are evaluated by various simulated results test scenarios in Sections V, which further examine the accuracy and efficacy of the recommended operating systems

2. Evaluation of the Rcg Approach

A GCC's overall infused current, I may be described in perspective of its watt/wattles and +ve/-veelements as

$$i = i_p + i_q = i_p^+ + i_p^- + i_q^+ + i_q^-$$

here the vectors having superscripts "+"/"" as well as subscripts "p"/"q" represent the real/reactive and positive/negative portions, accordingly. The standard positive or negative and real or reactive currents may be set variably to supply the optimum operating performance of an GCC in a variety of scenarios, such as different uneven faults, coding constraints, and line characteristic impedance. The entire baseline current may be calculated by combining four elements (positive or negative and active or reactive) in the following manner:

$$\begin{split} i_p^+ &= k_p \frac{P^*}{(V^+)^2} v^+ = K_p^+ v^+ i_p^- = \left(1 - k_p\right) \frac{P^*}{(V^-)^2} v^- = K_p^- v^- \\ i_q^+ &= k_q \frac{Q^*}{(V^+)^2} v_\perp^+ = K_q^+ v_\perp^+ i_q^- = \left(1 - k_q\right) \frac{Q^*}{(V^-)^2} v_\perp^- = K_q^- v_\perp^-. \end{split}$$

3. Technique of Optimal Support Proposed When the optimum phase current, I limit, is not



1) lower real power oscillations; 2) lower reactive energy oscillations; 3) lower glitch current; 4) Elixir of maximum possible reactivepowerand5) allowable maximum injection of real power In the following part, a sophisticated approach is described, it also includes the greatest permissible watt power i/p but then also commands the voltage levels inside the acceptable limitations.

4. VSS-MAP

Another significant goal that is addressed in this study is the support of the PCC voltage through the use of DG units. If the DG plants regard power and network impedance are not too low, the three-phase voltages can be controlled at the required range between Vmin and Vmax even with considerable sagsWhen it comes to voltage support, the main need is to prevent overvoltage and undervoltage at the PCC wherever feasible. However, a suitable solution can be found within this range to meet other objectives as well. This article, unlike [14], addresses the watt components of the current. Maintaining voltage limitations during unbalanced grid failures may be expressed as

$$V_{abc-max} = max\{V_a, V_b, V_c\} \le V_{max}$$

$$V_{abc-min} = min\{V_a, V_b, V_c\} \ge V_{min}$$

5. Simulation Results

A. MOP and MOQ

The numerical model of two of the suggested approaches, MOP and MOQ. kp&kq are both set to 1 in normal operation, resulting in pure positive sequence current injection [2]. The results are obtained by the use of mesh failures, in which a 1-ph-to-GF is modeled and the PCC voltage deteriorates, as shown in Fig. 1.

During t1 = 0.30 s and t2 = 0.60 s, a large voltage drop occurs at Va = 0.50 pu. In addition, after t2 = 0.60 s, where Va is virtually zero, a solid 1-ph fault is 533



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emulated for additional analyses. P and Q are set to .100 MW and 0.30 MVar in this test case, respectively. kp&kq are not limited to "1" and are computed using (13) and (14), respectively. After employing the MOP (at t = 0.400.50 s and t = 0.700.80 s) and MOQ (at t = 0.500.60 s and t = 0.801.0 s) techniques, the swings on the watt and wattles powers are abolished.

B.MFC

The outcome of the proposed MFC technique is investigated in this test scenario. To reduce the fault current, the best kp value is given using the suggested equations in Section III-C as kp = 0.79. Fig. 2 depicts the outcome of using the MFC method at t = 0.6 s



C.MAP

It investigates and investigates the suggested equations for the process of MAPbelow various fault situations. wield (14)–(17), the large reference P is found when all 3-ph currents are min than the current's preset large value. The results of the MAQ process are not given here due to space constraints. These findings are identical to those of the MAP approach, with the exception that the largewattles power in the MAQ is defined by (18) - (20).

D.VSS-MAP

scenario demonstrates the viability of the suggested VSSMAP concept. To clearly show the performance of the suggested VSS approach, a 0.050 delay after all fault occurrences is employed to compare the results before and after the VSS strategy is implemented. Figure 3 demonstrates how this method keeps all three phases within the intended range of Vmin = 0.9 p.u. and Vmax = 1.10 p.u. After t = 0.40 s, the voltage sag in phase A is 0.250 p.u. (0.150 p.u. below Vmin), therefore Va by 0.150 p.u. will result in overvoltage in the other 2 stages. The VSS system is employed to inject both -ve and The VSS system is employed to inject both -ve and Fig. 4 further illustrates that the MAP technique computed the maximum watt power when the 3-ph currents are within the predefined limitations, i.e., $I_{\text{limit}} = 200 \text{ A}$, in addition to exhibiting the VSS process. As a consequence, the three objectives of both methods (as specified in part IV) are satisfied at the same time in this test case.



Figure 4.VSS-MAP method



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CONCLUSION

This work provided optimal reference current generating procedures by infusing an appropriate set of +ve/-ve watt/wattlescurrents using four regulating factors. Analytical formulas were provided to find the best value of these parameters under all network voltage conditions. The recommended techniques aim to control three-phase voltages, lessen power swing, cut fault currents, and provide big power delivery in low-voltage and unbalanced situations. These optimal performances provide important advantages for increasing GCC penetration, including improved capacity, reduced dc-link wave, improved stability of the ac network, adherence to mesh standards. and tight avoided equipment tripping. The results of simulation were used to validate the beneficial recommended solutions' outcomes.

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